

Article

Electrodissolution of Cu-Zn Alloys in Acetate Media

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A eletrodissolução de ligas de Cu-Zn, de diferentes composição química (CuZn37 e CuZn39Pb3) foi estudada em solução tampão de acetato, pH 5, através de medidas de potencial de circuito aberto e voltametria cíclica, sob condições estáticas e dinâmicas. A menor resistência à corrosão detectada nestas ligas, comparativamente ao Cu puro, foi atribuída à estrutura da camada anódica formada $ZnO \cdot x H_2O / Cu_2O-CuO$, a qual apresenta menor proteção que a camada Cu_2O-CuO , formada sobre o eletrodo de Cu puro. Não foi observada a dissolução seletiva do Zn, verificando-se a dissolução simultânea dos constituintes das ligas. A velocidade de eletrodissolução das ligas neste meio, mostrou-se superior à do Cu puro e inferior à do Zn puro.

The electrodisolution of Cu-Zn alloys with different chemical compositions (Cu37Zn and Cu39Zn3Pb) in acetate buffer pH 5 was studied by means of corrosion potential measurements and cyclic voltammetry, under static and dynamic conditions. The lower corrosion resistance of the brass in comparison to pure Cu, was attributed to the anodic layer structure consisting of a complex $ZnO \cdot x H_2O / Cu_2O-CuO$ layer, which is less protective than the Cu_2O-CuO passive layer produced onto Cu. No selective dissolution of Zn was detected at both alloys, being their electrodisolution rate higher than that of pure Cu and smaller than that of pure Zn.

Keywords: brass, dezincification, acetate media

Introduction

The electrochemical behaviour of Cu-Zn alloys in different environments has been extensively studied over a wide range of experimental conditions¹⁻³. It depends on the alloy composition, the distribution of Cu and Zn oxides and their atomic species at the alloy surface, solution composition, surface pre-treatment and temperature. The study of the corrosion and passivation of these alloys (named brass) has been particularly oriented towards dezincification and stress corrosion cracking of this material. Dezincification is a well-known dealloying process by which the preferential dissolution of the Zn component takes place leaving a porous residue rich in Cu. Conversely, the brass loses its valuable physical and mechanical properties, leading to structural failure. The dezincification of α -, β -, and $(\alpha+\beta)$ -brass was studied comparatively in sulphuric acid solution. The obtained data indicate that the corrosion of α -brass is remarkable and resulted in the

depletion of Cu, whereas the $(\alpha+\beta)$ -brass revealed galvanic dezincification³. In alkaline media Morales *et al.*⁴ found that the corrosion resistance increases in the following order $(\alpha+\beta)$ -brass \cong β -brass $<$ α -brass.

The exact mechanism of the Zn selective dissolution is not completely understood, however there was reasonable correlation between the effect of the brass crystallographic structure and the dezincification. In this connection, the addition of an alloying element such as Sb, Al or Pb has been proposed to increase the brass corrosion resistance. In the case of leaded brass, the presence of Pb improves the machinability of the brass⁵.

Although much work has been devoted on this subject, very little information have been reported concerning the brass dissolution mechanism in nearly neutral aqueous solutions containing acetate anion. A general survey on the literature indicates that despite the scarce data available on this subject, the acetate presence enhances the corrosion rate of copper^{6,7} and also that stress corrosion cracking and generalised corrosion can be induced in α -brass by sodium acetate⁸.

The present work is devoted to the investigation of the electrochemical behaviour of two $(\alpha+\beta)$ -brasses, with

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different chemical compositions (Cu₃₇Zn and Cu₃₉Zn₃Pb) in aqueous sodium acetate (Ac) buffer pH 5, by means of corrosion potential measurements and cyclic voltammetry, under static and dynamic conditions. The effect of Pb on the corrosion rate of the brass was studied.

Experimental

Measurements were made on Cu (99.999% purity), Zn (99.999% purity) Cu₃₇Zn and Cu₃₉Zn₃Pb rotating disc electrodes axially embedded in a Teflon holder to offer a flat disc shaped surface of 0.0314 cm² geometric area, which could be used either still or under rotation. The pure metals are from Aldrich and the brasses from Goodfellow. The electrodes were polished with 600, 1200 and 2400 grit water-papers, degreased with etanol p.a. and rinsed with twice-distilled water.

A saturated calomel electrode (SCE) provided with a Luggin capillary tip, was used as reference electrode and all potentials were referred to this electrode. A large platinum wire was used as counter-electrode, inserted in a glass tube ended by a filter glass. The three-electrodes were mounted in a conventional glass cell. Experiments were carried out with sodium acetate aqueous solutions (0.1 and 1 mol L⁻¹ Ac) and the pH was adjusted to 5 using glacial acetic acid. Electrolytes were prepared from analytical grade reagents and twice-distilled water. All solutions were deaerated by bubbling with N₂ for 10 minutes prior to any measurement and were purged continuously throughout the experiment. The temperature was maintained at 298K.

Voltammetric measurements were made by using a Bipotentiostat EG&G PAR model 366 and an analytical rotator EG&G PAR model 616.

Results and Discussion

Figure 1 shows the variation of the open-circuit potential (E_{corr}) with time, over a period of 60 minutes, for the different alloys, Cu and Zn electrodes in 0.1 mol L⁻¹ Ac buffer pH 5, under static conditions. The E_{corr} for Cu electrode remains in the metal active zone, where Cu (I) is stable⁹. Concerning the Zn electrode the E_{corr} remains also in the active zone of this metal⁹. The open-circuit potential value for Cu₃₇Zn alloy is more negative than that of pure Cu. There is a linear E_{corr} /time relation rise with a slightly negative slope, which reaches a steady state value after 10 minutes. In the case of Cu₃₉Zn₃Pb the open-circuit potential corresponds to thermodynamic potential range where Pb (II) is stable, meaning that the preferential dissolution of Pb takes place⁹. The presence of Pb as a separate phase in the (α + β)-brass microstructure explains the close relation between these values. Similar results were reported for leaded brass in a phosphate buffer, pH 7⁵.

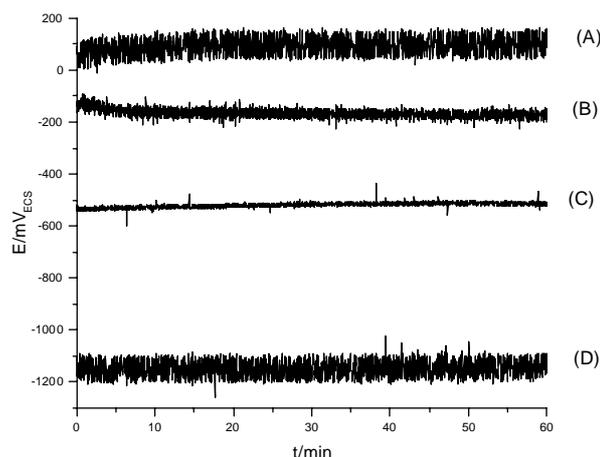


Figure 1. Variation of the corrosion potential (E_{corr}) with immersion time in 0.1 mol L⁻¹ Ac solution, pH 5 at $\omega = 0$ rpm, for Cu (A), Zn (B), Cu₃₇Zn (C) and Cu₃₉Zn₃Pb (D) disc electrodes.

Potential oscillations were detected during the measurements for all working electrodes. According to thermodynamic data, the open-circuit potential value for each specimen corresponds to the metal active zone. So, this feature can be attributed to a dissolution/precipitation process taking place at the electrode surface, as soon as it was immersed in the acetate solution. These findings are in agreement with what has been obtained for Cu-based alloys in alkaline media by Hurtado *et al.*¹⁰. Observations of potential transient fluctuations under galvanostatic control and open circuit conditions, or of current transient fluctuations under potentiostatic control is a well-documented feature of the metal corrosion¹¹. Oscillations observed from the oxidation of metals are directly linked to specific conditions of potential, hydrodynamics and electrolyte composition. Keiser and Cherson¹² have detected voltage oscillations for Fe in H₂SO₄. They proposed a theory which involves the coupling between the electric field and reducible species diffusion near the electrode surface and includes certain effects of double layer relaxation. On the other hand, theoretical treatments point out that the oscillatory nature of the potential transients can be related to the coexistence of a multiplicity of steady states¹³.

Open-circuit potential shifting to more negative values is observed for Cu⁷ in 1M Ac solution and to more positive values for Cu₃₉Zn₃Pb. The leaded brass reaches a steady-state potential of -0.49V after 50 minutes of immersion. On increasing acetate concentration, the Zn and Cu₃₇Zn corrosion potential values remain unaltered (not shown here). This means that at the open-circuit potential these specimens reach a pseudo steady-state, independent of the acetate concentration¹⁴. Based upon these data (Figure 1) it can be concluded that at the open-circuit potential, the selective dissolution of Zn, at both brasses, was not

observed, whereas the simultaneous dissolution of the alloy components takes place.

For the Cu electrode, data obtained in previous work⁷ showed that the E_{corr} shifts to more negative values under electrode rotation. Thus, on increasing the mass transport rate, the Cu (I) species flux into the solution increases exposing the bare metal to further dissolution shifting E_{corr} to more negative values. Feng *et al.*¹⁵ reported a similar E_{corr} dependence with rotation speed for copper in sulphate solutions at pH 5. Their results have been explained by assuming that still solutions favour the deposition of Cu (I) species at the metal-solution interface due to the Cu_2O low solubility. Electrode rotation has no effect on the open-circuit potential of Zn electrode (data not shown).

In order to investigate the effect of electrode rotation on the open-circuit potential, experiments were carried out at 500 rpm (Figure 2). In the case of the Cu37Zn brass, electrode rotation produces no changes on the E_{corr} value, however the oscillatory behaviour enhances. So, at the open circuit potential, for Cu37Zn and Zn electrodes, the process is independent of mass transport, being limited by an electrochemical step¹⁴ (charge transfer, adsorption, surface chemical reaction, etc.). A distinct behaviour was detected at the Cu39Zn3Pb specimen: on increasing the mass transport rate, the E_{corr} shifts to more positive values. These features seem to indicate that a topochemical process takes place at the leaded brass surface¹⁶, being dependent on electrode rotation. The E_{corr} /time profiles show that the oscillations enhanced under dynamic conditions. These features were previously observed for Cu rotating disc electrode in chloride¹⁷ and in acetate media¹⁸ under potentiodynamic conditions. According to reference 18 once the oscillations began, they could be stopped (and restarted) by adjusting the potential and/or the rotation rate. There is an agreement in the literature that specific conditions including the metal surface morphology, film thickness, composition and structure, are generally associated with the existence and structure of a particular type of oscillatory behaviour. The dezincification produces a porous layer onto the brass surface, enhancing the electrochemical oscillations¹⁹.

The effect of acetate concentration on the copper cyclic voltammograms run from $E_{\text{sc}} = -1.0\text{ V}$ to $E_{\text{sa}} = 1.0\text{ V}$, at 0.001 V s^{-1} sweep rate, with stationary electrode in 0.1 mol L^{-1} Ac (solid line) and 1 mol L^{-1} Ac (dashed line) solutions is shown in Figure 3. The anodic scan in 0.1 mol L^{-1} Ac exhibits three peaks A_1 , A_2 and A_3 followed by a sharp current decrease until a minimum value (0.2 mA cm^{-2}) around 0.5 V . This potential was assigned as the Flade potential (E_{F}) similarly to what has been previously reported²⁰. In the reverse direction of the scan a reactivation of the

electrooxidation process is observed at the same potentials of the forward scan, followed by a small cathodic peak C_1 located at -0.2 V . This behaviour was also described by Drogowska *et al.*²¹ for copper in bicarbonate solution indicating that the metal is highly soluble despite the fact that the electrode surface remains covered by a film. On increasing acetate concentration (dashed line) the potential of the anodic peaks and also the E_{F} shifts toward more negative values indicating that the dissolution/precipitation processes are anticipated. At more concentrated acetate solutions a sharp current increase is observed at the rising portion of peak A_1 suggesting that the film becomes less protective. According thermodynamic data⁹ these anodic processes can be ascribed to a first oxidation process from Cu (0) to Cu (I) followed by a second stage yielding Cu (II) as already reported in the literature²².

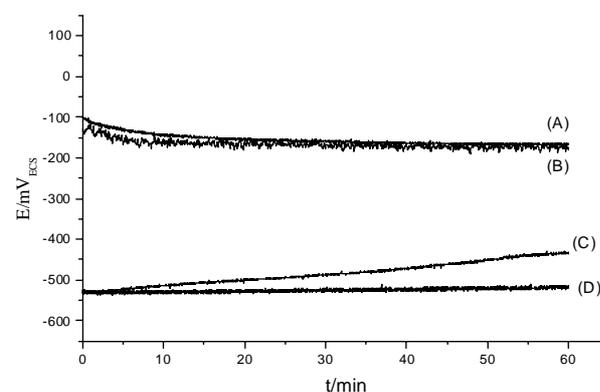


Figure 2. Variation of the corrosion potential (E_{corr}) for the alloys electrodes with immersion time in 0.1 mol L^{-1} Ac solution, pH 5 under electrode rotation: (A) Cu37Zn at $\omega = 0\text{ rpm}$ (B) Cu37Zn at $\omega = 500\text{ rpm}$, (C) Cu39Zn3Pb at $\omega = 0\text{ rpm}$ and (D) Cu39Zn3Pb at $\omega = 500\text{ rpm}$.

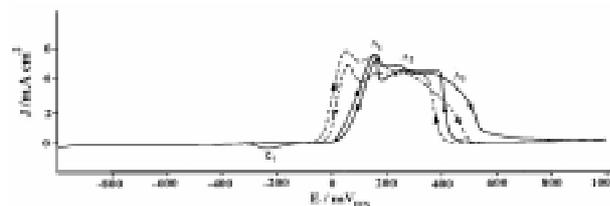


Figure 3. Influence of acetate concentration on voltammograms obtained with a Cu disc electrode, between $E_{\text{sc}} = -1.0\text{ V}$ and $E_{\text{sa}} = 1.0\text{ V}$ at 0.001 V s^{-1} , under static conditions: (—) 0.1 mol L^{-1} Ac solution, (---) 1 mol L^{-1} Ac solution.

The voltammogram obtained with a Zn electrode under static conditions (Figure 4) in 0.1 mol L^{-1} Ac shows an abrupt current increase when the potential is shifted positively. The reverse potential scan presents a small cathodic peak at -0.8 V , which can be assigned to the electroreduction of Zn^{+2} , taking place simultaneously with the HER⁴.

In 1 mol L⁻¹ Ac the anodic scan exhibits an intense dissolution process and no cathodic peak was detected at the reverse scan (data not shown).

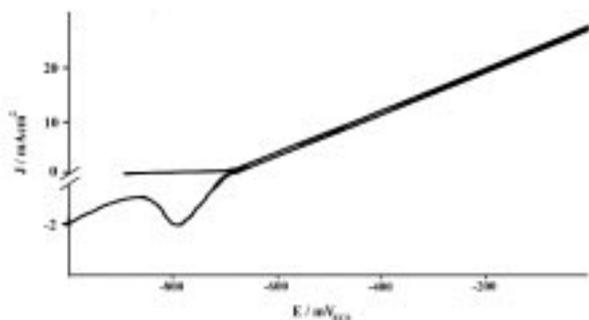


Figure 4. Voltammogram obtained with a Zn disc electrode in 0.1 mol L⁻¹ Ac solution, between $E_{sc} = -1.0$ V and $E_{sa} = 1.0$ V at 0.001 V s⁻¹ and under static conditions.

Figure 5 shows the effect of acetate concentration on the cyclic voltammograms for both alloys, run from $E_{sc} = -1.2$ V to $E_{sa} = 1.0$ V, at 0.001 V s⁻¹ sweep rate, under static conditions. On increasing the acetate concentration the alloys dissolution rate increases. For Cu37Zn in 0.1 mol L⁻¹ Ac the anodic scan exhibits a peak at ca 0.6V which can be related to the formation of cupric species. The potential scan in the negative direction presents an intense reactivation process followed by a cathodic peak at -1.0V. The shape of the Cu37Zn voltammetric curve changes in 1 mol L⁻¹ Ac solution, indicating that a less resistive film was formed. The anodic peak is anticipated, similarly what has been observed with pure Cu (see Figure 3). The cathodic scan shows the presence of a reactivation process, followed by a cathodic peak at -0.5V that can be related to the electroreduction of copper. The anodic to cathodic charge ratio is always greater than the unity revealing that the alloy dissolution is the main process.

The Cu39Zn3Pb voltammograms exhibit an intense dissolution process. No film formation was detected in 0.1 mol L⁻¹ Ac. On increasing acetate concentration an hysteresis is observed at more positive potentials. The negative going scan presents three cathodic peaks located at -0.25V, -0.48V and -0.90V, respectively. The electroreduction processes involving cuprous and cupric species originate the peaks at -0.25V and -0.48V. The peak at -0.90V is assigned to the Zn electroreduction and the HER⁴. These voltammograms indicate that the structure and/or composition of the anodic layer is dependent on the acetate concentration. The most remarkable feature is that at similar experimental conditions, the dissolution rate at the leaded brass in 0.1 mol L⁻¹ Ac is smaller than that observed at the Cu37Zn. However, in more concentrated solution (1 mol L⁻¹

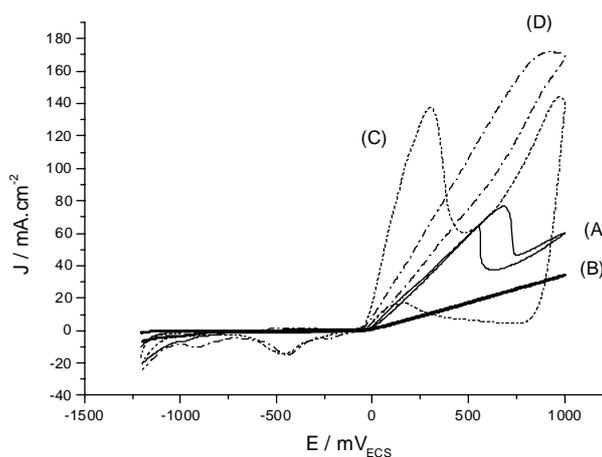


Figure 5. Influence of acetate concentration on voltammograms obtained with the alloys disc electrodes, between $E_{sc} = -1.0$ V and $E_{sa} = 1.0$ V at 0.001 V s⁻¹, under static conditions: (A) Cu37Zn in 0.1 mol L⁻¹ Ac solution, (B) Cu37Zn in 1 mol L⁻¹ Ac solution, (C) Cu39Zn3Pb in 0.1 mol L⁻¹ Ac solution and (D) Cu39Zn3Pb in 1 mol L⁻¹ Ac solution.

Ac) the corrosion rate for both alloys decreases abruptly, even for the leaded brass. So, the corrosion resistance of the Cu-Zn alloys studied was lower than that of pure Cu, but considerably greater than that of pure Zn. It must be emphasised that the leaded brass presents a higher percentage of more active components in the alloy ($\approx 42\%$) if compared with the Cu-37Zn brass.

Therefore the voltammograms run in still solutions, keeping constant the switching potentials, change with acetate concentration. The anodic to cathodic voltammetric charge ratio is higher than 1 for all acetate concentrations. Electrode rotation produces no changes on the brass voltammograms (data not shown).

Previous work on the electroreduction of copper in acetate media concluded that the mechanism involves a sequence of competitive and parallel reactions giving rise to a duplex film on the metal surface, whose nature and composition are dependent on the acetate concentration and time of polarisation^{7,18}.

To gain further information about the electroreduction of these alloys the effect of the sweep rate on the electroreduction was analysed. The sweep rate (v) effect on Cu37Zn voltammograms in 0.1 mol L⁻¹ Ac solution obtained under static conditions, run from $E_{sc} = -1.2$ V to $E_{sa} = 1.0$ V, is shown in Figure 6. The anodic to cathodic charge ratio is practically v -independent, being higher than unity, in the entire range of v employed in this study. So, it can be concluded that the anodic process is mainly alloy dissolution and only a fraction of the anodic layer can be electroreduced. This behaviour was also observed with less concentrated acetate solution. The anodic layer resistance is not influenced by the polarisation time, similarly to what happens with pure Zn in this media.

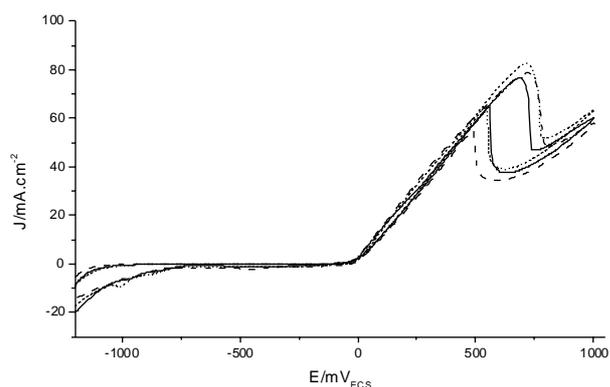


Figure 6. Influence of the sweep rate (v) on voltammograms obtained with a Cu37Zn disc electrode in 0.1 mol L^{-1} Ac solution, between $E_{sc} = -1.0 \text{ V}$ and $E_{sa} = 1.0 \text{ V}$ at $v = 0.01 \text{ V s}^{-1}$ (—), $v = 0.02 \text{ V s}^{-1}$ (....), $v = 0.05 \text{ V s}^{-1}$ (---).

Figure 7 points out the effect of v on the Cu39Zn3Pb-brass voltammograms. The broad and asymmetric anodic peak observed around -0.30 V , during the positive going scan enhances as v increased, whereas the anodic to cathodic current crossover potential becomes v -independent. These features seem to indicate that the anodic thickening layer is determined by the diffusion of reactants through the growing film. Again, these findings are an indication that a change in the structure and /or composition of the anodic layer takes place on changing the time of polarisation, similarly what was described for pure Cu⁷. Moreover the Pb dissolution is favoured when high sweep rates ($v \geq 0.050 \text{ V s}^{-1}$) are employed²². So, under this condition, the dissolution/precipitation of Pb^{+2} on the electrode surface can seal uncovered active sites and improve the anodic layer resistance.

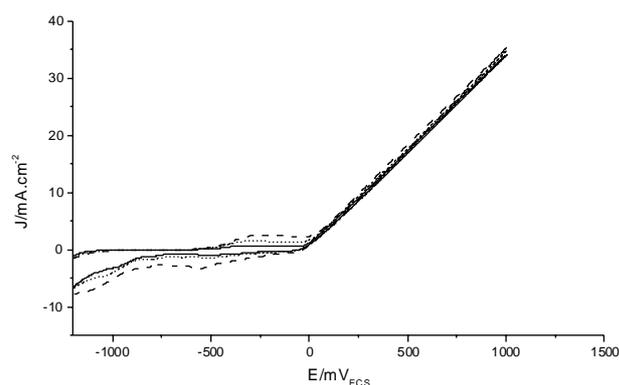


Figure 7. Influence of the sweep rate (v) on voltammograms obtained with a Cu39Zn3Pb disc electrode in 0.1 mol L^{-1} Ac solution, between $E_{sc} = -1.0 \text{ V}$ and $E_{sa} = 1.0 \text{ V}$ at $v = 0.01 \text{ V s}^{-1}$ (—), $v = 0.02 \text{ V s}^{-1}$ (....), $v = 0.05 \text{ V s}^{-1}$ (---).

The lower corrosion resistance of the brass in comparison to pure Cu, can be attributed to the anodic layer

structure consisting of a complex $\text{ZnO} \cdot x \text{ H}_2\text{O} / \text{Cu}_2\text{O} - \text{CuO}$ layer, which is less protective than the $\text{Cu}_2\text{O} - \text{CuO}$ passive layer produced onto Cu. A comparison between the alloys and pure Cu voltammetric curves, point in relief that the anodic layers formed on brass, are porous and under diffusion control²³.

The structure of the anodic layer formed onto Cu electrode in acetate was previously studied using RRDE experiments²⁴. The obtained results point out that the faradaic process occurring at the Cu disc involves the formation of both insoluble and soluble Cu (I) and Cu(II) species. The small current due to Cu (II) at the ring could indicate that these species are complexed by adsorbed acetate at the disc surface. Further, tabulated data show that the cupric acetate has a low solubility in water⁶ which reinforces the idea of the copper complex formation. According to Stulikova *et al.*²⁵ the voltammetric curves of Cu (II) in acetate media at a glassy carbon electrode seem to depend on a great extent on the degree to which monovalent copper, produced in an electrochemical reaction, remains adsorbed on the electrode surface to undergo further electrochemical reactions. Probably the adsorption/desorption equilibrium of the intermediate Cu (I) in copper dissolution is altered by the presence of adsorbed acetate on the metal surface. This assumption is consistent with what has been reported in various investigations^{26,27}.

Based upon the voltammetric experiments and in analogy with the data reported for Cu electrode it is possible to postulate the participation of the acetate anion in the film formation process. It follows from the brass cyclic voltammograms that the alloys mechanism dissolution is dependent on the applied potential : at low anodic overpotential the preferential dissolution takes place, being the simultaneous dissolution dominant at higher anodic overpotential .

Conclusion

From the open-circuit measurements and the voltammetric data it was possible to characterise the distinct behaviour of the Cu37Zn and Cu39Zn3Pb alloy. The open-circuit potential of these alloys occurs at potentials more negatives than that of pure Cu and markedly more positive than that of Zn. The open-circuit potential is independent on acetate concentration for both alloys, whereas the electrode rotation shifts the Cu39Zn3Pb potential to more noble values.

From the voltammetric data it is proposed that the anodic layer formed at more positive potentials, consists of $\text{ZnO} \cdot x \text{ H}_2\text{O} / \text{Cu}_2\text{O} - \text{CuO}$, which is influenced by acetate concentration. Under the experimental conditions used in

this work no selective dissolution of Zn was detected at both alloys, being their electrodisolution rate higher than that of pure Cu and smaller than that of pure Zn. The preferential dissolution of Zn was detected, although the simultaneous dissolution of the brass components takes place at both alloys, in accordance with their chemical composition.

Acknowledgements

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References

1. Langenegger, E. E.; Calladhan, B. G. *Corrosion*, **1972**, 28, 245.
2. Lee, C. K.; Shih, H. *Corrosion* **1996**, 52, 141.
3. El-Egamy, S. S.; El-Azab, A. S.; Badawy, W. A. *Corrosion* **1994**, 50, 468.
4. Morales, J.; Fernandez, G. T.; Esparza, P.; Gonzalez, S.; Salvarezza, R. C.; Arvia, A. J. *Corros. Sci.* **1995**, 37, 211.
5. Al-Kharafi, F. M.; Badawy, W. A. *Mater. Sci. Forum* **1998**, 289, 471.
6. Dewald, H. D.; Parman, P.; Rollins, R. W. *J. Electroanal. Chem.* **1991**, 306, 297.
7. Schmidt, A. M. *Thesis*, Universidade Federal do Rio Grande do Sul, 1997.
8. Parkins, R. N.; Holroyd, N. J. H. *Corrosion* **1982**, 38, 245.
9. Pourbaix, M. *Atlas of Electrochemical Equilibria in Aqueous Solutions*, NACE, Houston, 1974.
10. Hurtado, M. R. F.; Sumodjo, P. T. A.; Benedetti, A. V. *J. Electrochem. Soc.* **1993**, 140, 1567.
11. Burnstein, G. T.; Pistorius, P. C.; Mattin, S. P. *Corros. Sci.* **1987**, 57, 289.
12. Keizer, J.; Scherson, D. *J. Phys. Chem.* **1980**, 84, 2025.
13. Sharland, S. M. *Corros. Sci.* **1987**, 27, 289.
14. Power, G. P.; Ritchie, I. M. *Electrochim. Acta*, **1981**, 26, 1073.
15. Feng, Y.; Siow, K. S.; Teo, W. K.; Hsieh, A. K. *Corrosion* **1997**, 53, 389.
16. Gileadi, E.; Kirowa-Eisner, E.; Penciner, J. *Interfacial Electrochemistry. An Experimental Approach*, Addison-Wesley Publis. Comp., Inc., Massachusetts, 1975.
17. Lee, H. P.; Nobe, K.; Pearlstein, A. J. *J. Electrochem. Soc.* **1985**, 132, 1031.
18. Dewald, H. D.; Parmananda, P.; Rollins, R. W. *J. Electrochem. Soc.* **1993**, 140, 1969.
19. Badawy, W. A.; Al-Kharafi, F. M. *Corrosion* **1999**, 55, 268.
20. Mostafa, S. N.; Mourad, M. Y.; Seliman, S. A. *J. Electroanal. Chem.* **1981**, 130, 221.
21. Drogowska, M.; Brossard, L.; Ménard, H. *J. Appl. Electrochem.* **1994**, 24, 344.
22. Kremer, E.; Azambuja, D. S. *J. Braz. Chem. Soc.* **1997**, 8, 165.
23. Calandra, A. J.; Taconi, N. R.; Pereiro, R.; Arvia, A. J.; *Electrochim. Acta* **1974**, 19, 901.
24. Schmidt, A. M.; Azambuja, D. S. *Corros. Sci.* "submitted for publication".
25. Stuliková, M.; Vydra, F. *J. Electroanal. Chem.*, **1973**, 44, 117.
26. Sander, U.; Strehlow, H. -H.; Dohrmann, J. K. *J. Phys. Chem.* **1981**, 85, 447.
27. Coulter, P. D.; Iwamoto, R. T. *J. Electroanal. Chem.*, **1967**, 13, 21.

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