

Microstructure and Mechanical Properties of Gypsum Composites Reinforced with Recycled Cellulose Pulp

Magaly Araújo Carvalho^{a*}, Carlito Calil Júnior^a, Holmer Savastano Junior^b,

Rejane Tubino^c, Michele Tereza Carvalho^d

^aEscola de Engenharia de São Carlos, EESC/USP – São Carlos - SP, Brazil

^bFaculdade de Zootecnia e Engenharia de Alimentos, FZEA/USP, Pirassununga - SP, Brazil

^cEscola de Engenharia Civil, EEC/UFG – Goiânia - GO, Brazil

^dFurnas Centrais Elétrica – Goiânia - GO, Brazil

Received: May 20, 2007; Revised: October 17, 2008

The use of waste fibers for the reinforcement of brittle matrices is considered opportune for the sustainable management of urban solid residues. This paper examines the microstructure and mechanical properties of a composite material made of gypsum reinforced with cellulose fibers from discarded Kraft cement bag. Two different kinds of gypsum were used, natural gypsum (NG) and recycled gypsum (RG), both with an addition of 10% by mass of limestone. For the production of samples, slurry vacuum de-watering technique followed by pressing was evaluated revealing to be an efficient and innovative solution for the composites under evaluation. The composite was analyzed based on flexural strength tests, scanning electron microscopy (SEM) imaging, secondary electron (SE) detection, and pseudo-adiabatic calorimetry. The morphology of the fractured surfaces of flexural test samples revealed large gypsum crystals double the original size surrounding the fibers, but with the same overall aspect ratio. Natural fibers absorb large amounts of water, causing the water/gypsum ratio of the paste to increase. The predominance of fiber pullout, damaged or removed secondary layers and incrustated crystals are indicative of the good bonding of the fiber to the gypsum matrix and of the high mechanical resistance of composites. This material is a technically better substitute for the brittle gypsum board, and it stands out particularly for its characteristics of high impact strength and high modulus of rupture.

Keywords: gypsum-cellulose composite, waste fibers, recycled pulp, mechanical properties

1. Introduction

The productive chain of the civil construction industry has represented one of the activities of the society which has interfered most directly with the environment. It is a large consumer of resources (materials/energy), highly polluting (emission of CO₂), and a generator of residues. Therefore, in the search of a sustainable construction, attentions turn to research on agglomerates of minor energetic consumption and to the adequate use of industrial and agro-industrial waste. When compared to cement and lime, the industrial process of plaster production issues less anhydrous carbon (CO₂) and reveals the lowest energy consumption, being thus regarded as “green agglomerate”. However, studies carried out in this country indicate that the waste indexes of this material reach around 45% of the total dough¹.

The combination of inorganic binder material such as gypsum with waste fibers has been considered an interesting option for material recycling and has been used for structural overlays and ceilings in several parts of the world². The main advantage of using natural fibers is their high energy-absorbing capacity resulting from their low modulus of elasticity. When fiber pullout predominates over fracture, fiber-matrix bonding is considered the main factor influencing the composite's toughness³, ensuring the possibility of post-fracture work, which is an important characteristic in civil construction. The high availability of noncommercial fiber waste⁴, or low cost fibers, may constitute a good opportunity for a serious proposal of sustainable methods for producing low cost gypsum-fiber components for civil

construction. Compared to composites reinforced with virgin fibers, composites containing recycled fibers have presented good mechanical properties. Research by Savastano Jr. et al.⁵ showed that banana pulp, *Eucalyptus grandis* and sisal wastes presented satisfactory adhesion in fiber-cement composites, reaching a flexural strength of 15.5 to 16.5 MPa. The sensitivity of natural fiber to the alkaline environment produced by the hydration of standard Portland cement with a pH of around 13 has led researchers^{6,7} to suggest the use of gypsum, with its pH of 7 to 8, as an adequate binder for matrices reinforced with alkaline-sensitive vegetal fibers.

The aim of this research was to examine the influence of cellulose pulp on the mechanical properties of construction gypsum. Moreover, the stirring vacuum de-watering process was evaluated for the production of composites. Savastano Jr Warden and Coutts⁸ previously studied and developed this technique for the production of composite materials based on cement matrices. The hydration kinetics and morphology of hardened paste are important parameters in understanding the material.

The hydration kinetics of gypsum occurs by an exothermic process of energy released in the form of heat. The microstructure of the paste changes in response to parameters such as hydration conditions, mixing water temperature, gypsum properties, and the application of chemical additives⁹. When gypsum is mixed with water, the supersaturated solution composed of SO₄²⁻ and Ca²⁺ ions precipitates into a needle-like crystalline network in a matter of minutes. Hardening be-

*e-mail: magaly@sc.usp.br

gins at the instant when the temperature gradient exceeds 0.1 °C/min and ends when the temperature reaches its maximum¹⁰. The reactivity of the hydration can be quantified based on calorimetric curves, i.e., on the velocity of heat radiation.

For the morphological analysis, fractured gypsum surfaces, with and without addition of cellulose pulp were prepared and visualised through a scanning electron microscope (SEM). The kinetics of the hydration process was assessed using a pseudo-adiabatic calorimeter.

2. Experimental

2.1. Materials

The materials used in this work were natural gypsum (NG), recycled gypsum (RG), limestone, Kraft paper pulp from discarded cement bags (cel-cb), and water (Figure 1).

The natural gypsum (NG) used in this research is a commercial product from the region of Grajaú, Maranhão state, Brazil, commercially available on the construction materials market, while the recycled gypsum (RG) originated from construction debris (dehydrated at 85 °C in a fan-assisted oven and milled for 20 minutes in ball-type mill). Table 1 lists the chemical composition and physical properties of the materials.

Calcium sulfates are the main components of gypsum. When treated with a diluted chloric acid solution they are expressed as sulfuric anhydride (SO₃) and calcium oxide (CaO), while impurities such as quartz are expressed as insoluble residues (RI). Clay minerals are quantifiable as aluminum (Al₂O₃) and iron (Fe₂O₃) oxide contents. Table 1 indicates that the products used here were of high purity grade, i.e., SiO₂+RI+Al₂O₃+Fe₂O₃ < 1.5%.

With regard to the calcium oxide content (CaO = 38.65%), the product fell within the standard limits. The sulfuric anhydride did not

meet the Brazilian standard¹¹, but lay within the limits established by the British¹² and French¹³ standards, which admit minimum values of respectively. Cincotto et al.¹⁴ analyzed 15 different types of Brazilian gypsum and concluded that a minimum value of 50% for SO₃ is sufficient to ensure gypsum quality.

Limestone is a raw material commonly employed by cement and fiber-cement manufacturers. The limestone used here came from the municipality of Cesarina, Goiás state, Brazil, and was supplied by Eternit Ltda. Its probable chemical composition is given in Table 2.

The limestone used here – an inert additive that facilitates drainage of the paste during molding – had a low fineness factor, with 67.5% of the particles sifting through a 100 mesh sieve, 18% through a 200 mesh sieve and 0.7% through a 325 mesh sieve. 17.3% of the particles were retained in the latter sieve and were added to the gypsum mass at a percentage of 10%.

The cellulose fibers of cement bag (cel-cb) were dispersed with water in a hydropulper, a giant industrial blender that separates particles, blending them into a homogeneous pulp. This preparation took place in the following stages: at a concentration of 6 g of Kraft paper per liter of potable water, the material was processed for 30 minutes (this period was established during the pulping process, since it resulted in the best pulp dispersion quality). After this dispersion process, the excess was drained off through a sieve and a fine strainer (causing the pulp to reaggregate). Lastly, the pulp, with a moisture content of about 75%, was again mixed for 5 minutes in a low speed laboratory electric mixer and stored in plastic bags in a refrigerator.

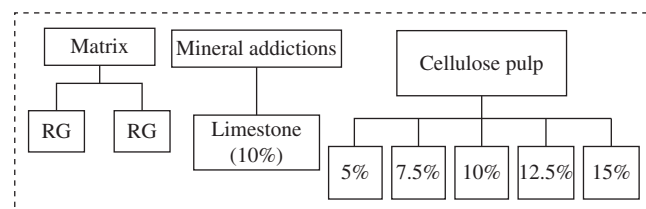


Figure 1. Flowchart of samples.

Table 2. Chemical composition of the limestone.

Properties	Content (%)
Loss to Fire	36.02
Silicon Dioxide (SiO ₂)	14.67
Calcium Oxide (CaO)	46.07
Magnesium Oxide (MgO)	0.53
Aluminum Oxide (Al ₂ O ₃)	0.90
Iron Oxide (Fe ₂ O ₃)	0.87
Total Alkalis	Content (%)
Sodium Oxide (Na ₂ O)	0.07
Potassium Oxide (K ₂ O)	0.09
Alkaline Equivalent	0.12

Table 1. Chemical and physical characteristics of the natural (NG) and recycled (RG) gypsum.

Properties		Standards - limits			Natural gypsum (NG)	Recycled gypsum (RG)
		NBR ^[9] 13207	BS ^[10] 1191/73	NFB ^[11] 12300/63		
Chemical analysis (%)	Water of crystallization	4.2 to 6.2	-	-	7.91	10.65
	CaO	>38	≥23.3	-	38.65	35.94
	SO ₃	>53	≥35	>45	52.08	49.61
	Al ₂ O ₃ + Fe ₂ O ₃	-	-	-	0.41	0.45
	SiO ₂ + RI	-	-	-	0.65	0.85
Calculated chemical percentage (%)	(CaSO ₄ ·1/2H ₂ O)	-	-	-	92.22	91.12
	(CaSO ₄)	-	-	-	-	-
	(CaSO ₄ ·2H ₂ O)	-	-	-	3.3	4.6
pH	-	-	-	7.96	8.12	
Physical properties	Specific mass (g.cm ⁻³)	> 700.00			2.50	2.56
	Unit mass (kg.m ⁻³)	> 1.10 (thick foundry gypsum)			649.00	504.73
	Thinness factor	< 1.10 (thin foundry gypsum)			0.72	1.54

The fibers were characterized in a Galai CIS-100 particle analyzer in the Federal University of Viçosa's Pulp and Paper Laboratory. This process consists of preparing a suspension of 0.001% of fibers in approximately 700 mL of water, allowing it to hydrate for 4 hours, and then circulating the suspension in the analyzer. The images are generated by a laser beam and measured by an analyzer using Wshape software. Table 3 summarizes the characteristics of the material.

2.2. *Stirring vacuum de-watering technique*

The composites were produced by the stirring vacuum de-watering process with the dispersion of solid materials in a large volume of water (in concentrations around 20% of solids by mass), vacuum drainage to remove excess of water (negative manometric pressure of 60 to 80 kPa), and pressing at 3.2 MPa for 5 minutes (Figures 2, 3 and 4).

The water/gypsum ratio – the difference in mass between the dry materials and the wet plate – was determined from the newly molded plates immediately after compression.

The plates were allowed to rest for 24 hours in the laboratory environment (at a temperature of 25 °C and air humidity of 75%), and then cured in a Termotron® chamber (at a temperature of 45 °C and relative humidity of 75%) until they attained a constant mass, which took 72 hours. Finally, the samples were dry-cut into 160 x 40 x 8 mm test specimens using a diamond disc saw (Figure 5).

2.3. *Mechanical behavior*

The samples' mechanical properties of the samples were analyzed based on flexural strength tests with four-point loading, following the recommendations of the RILEM Technical Committee 49 TFR¹⁵.

Table 3. Characteristics of the cellulose fibers of Kraft cement bag (cel-cb).

Pulp	Average length (mm)	Average width (µm)	Aspect ratio	Coarseness (mg/100 m)	Fibrous material/grams (millions)	Measured objects	Fine* (%)
cel-cb	0.80	22.67	35	23.65	5.31	11.712	52.43

*The fineness represents the percentage of fibers shorter than 0.07 mm of length, consequently, thus having a low capacity reinforcement of the matrix capacity.



Figure 2. Mixing in the blender.

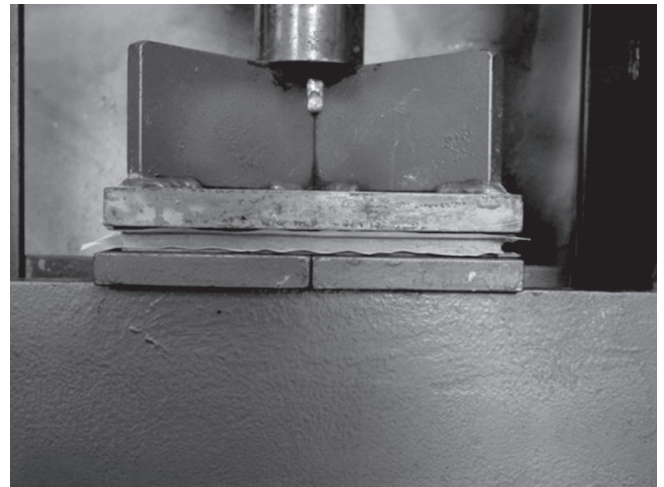


Figure 4. Mechanical pressing.



Figure 3. Mold.

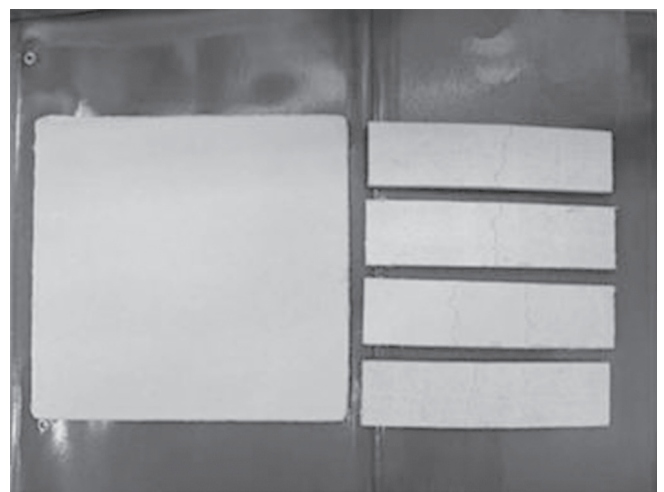


Figure 5. Cutting of the plates.

A universal EMIC DL 30000 testing machine was used with a 5 kN load cell and 1.5 mm/min compression arm displacement. The flexural properties of the materials were measured 14 days after manufacture. The results were calculated from the arithmetic average of a series of 12 test specimens.

The modulus of rupture (MOR) was calculated by the software M-Tests version 1.01/96 and given by the expression (1):

$$MOR = \frac{P_{max} \cdot l_v}{b \cdot e^2} \rightarrow MPa \tag{1}$$

The limit of proportionality (LOP) is given by the expression (2):

$$LOP = \frac{P_{LOP} \cdot l_v}{b \cdot e^2} \rightarrow MPa \tag{2}$$

The fracture toughness (T) was calculated by the integration of the load deflection curve to the point corresponding to a reduction in load carrying capacity to 50% of the maximum observed. It is given by the expression (3):

$$T = \frac{\text{fracture energy}}{b \cdot e} \rightarrow (kJ / m^2) \tag{3}$$

The modulus of elasticity (MOE) is given by the expression (4):

$$MOE = \frac{276 \cdot l_v^3}{1296 \cdot b \cdot e^3} \cdot \delta \rightarrow MPa \tag{4}$$

where:

- p_{max} = maximum load carried by the specimen (N);
- P_{LOP} = maximum applied load at which the load time (load-strain) curve deviates from linearity (N);
- l_v = the support span (mm);
- b = the specimen breadth (mm);
- e = the specimen depth (mm);
- δ = angular coefficient of linear domain of load x displacement curve.

2.4. Microstructure

The fracture surfaces were analyzed from samples fractured in the flexural strength test, using images obtained by scanning electron microscopy (SEM) with secondary electrons (SE). The maximum magnification used here was 3000x. The work distance (distance from the microscope’s lens to the test specimen) was about 20 mm and the accelerating voltage was 20 kV. The specimens were cut into prism shapes with 0.5 x 0.5 x 0.5 cm sides, attached to a sample holder and metallized with gold. The microscope used here was a Philips® model XL 30 FEG coupled to an EDAX Link Isis system for microanalysis.

2.5. Calorimetry

A pseudo-adiabatic calorimetry technique similar to that employed by Murat & Jeandot¹⁶, Hincapié & Cincotto¹⁷ and Antunes¹⁸ was applied to observe how the addition of limestone powder and cellulose pulp influenced the hydration of gypsum paste. This technique produces a temperature increment curve during the hydration of gypsum paste in relation to the beginning and end of the hardening process.

The variations in hydration-generated heat in the samples were measured with a pseudo-adiabatic calorimeter (Figure 6). The equipment consisted of a polystyrene foam cup to insulate the sample from room temperature, a thermocouple (copper-nickel), and Monitoring System Comtemp View® (version 1.05) software for temperature and

time readings. The materials and equipment were kept in a room with temperature set at 22 °C.

The sequence of the process was:

- 1 minute to add the gypsum powder to the pure water or to the water mixed with other materials (limestone and cellulose). The gypsum was poured into the insulated container through a funnel;
- 2 minutes for the gypsum powder to dissolve;
- 1 minute to homogenize the material (using a blade), and end of the mixing process; and
- Passive reading by the software.

The following samples were produced in this process: NG100 (composed of 100% natural gypsum); NG90+limestone (90% natural gypsum and 10% limestone); NG90+cel-cb (90% natural gypsum and 10% cel-cb); and NG80+limestone+cel-cb (80% natural gypsum, 10% limestone and 10% cel-cb).

3. Results and Discussion

3.1. Flexural behavior

Figure 7 and 8 depicts the strain displacement curves of the composites. The test specimens were composed of natural gypsum

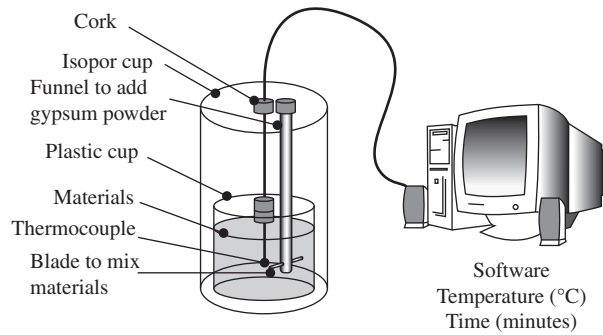


Figure 6. Pseudo-adiabatic calorimeter – equipment used in the laboratory to study the kinetics of gypsum hydration.

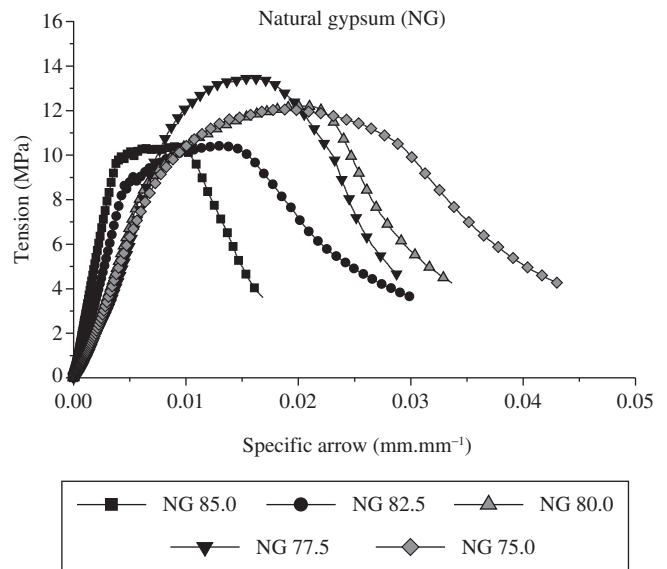


Figure 7. Strain displacement curves of matrices made of natural gypsum.

(NG), recycled gypsum (RG), 10% of added limestone, and different percentages (5, 7.5, 10, 12.5, and 15%) of Kraft cement bag pulp (celcb), and a reference sample without pulp.

The suction and compression-molding process produced composites with high mechanical performance. All the cellulose pulp waste (cel-cb) percentages improved the composites' mechanical performance. Composites containing 5% of pulp exhibited a two-fold improvement in performance, but the specimens with 12.5% of pulp (cel-cb) presented the highest flexural strength. Composites RG77.5 and NG77.5, with a 12.63 and 13.18 MPa modulus of rupture (MOR), presented an increase in resistance of 152% and 163%, respectively, compared to their counterparts without fibers, whose modulus of rupture was about 5.00 MPa (Table 4).

The specimens containing 12.5% of pulp (cel-cb) also presented the highest limit of proportionality (LOP), which is another indication that this was the ideal content. Under continuous loading, the LOP

indicates the maximum stress attained before the material exceeds the elastic state, i.e., before deviating from its linearity.

Table 4 indicates the absence of a direct correlation between increased mechanical strength and loss of toughness. With a pulp content of to 12.5%, the material showed an increase in toughness concomitant to the increase in the MOR.

3.2. Microstructure

The morphology of the gypsite crystals is the result of the conditions of paste hydration. Images of the composites molded by suction and compression exhibited significant variations in crystal size.

Compared with samples without pulp, the samples containing 10% of pulp showed varying gypsite crystal sizes around the fibers (Figure 9 and 10), although they maintained their original needle shape and arrangement. Dihydrate crystals are predominantly needle-shaped. The larger size of the crystals surrounding the fibers may be attributed to the number, shape and hydrophilic characteristics of the

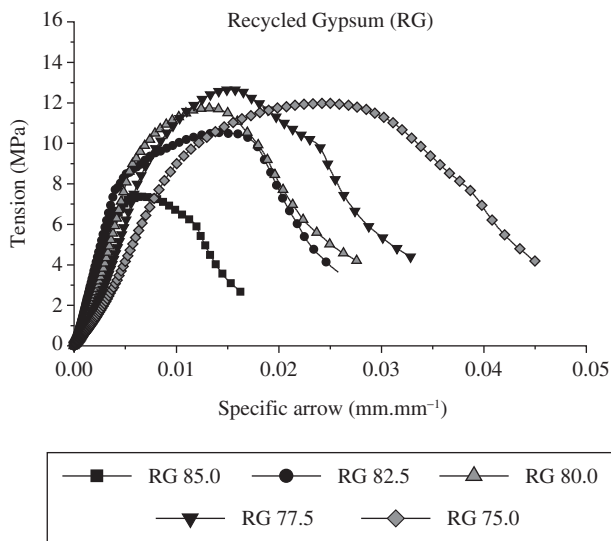


Figure 8. Strain displacement curves of matrices made of recycled gypsum.

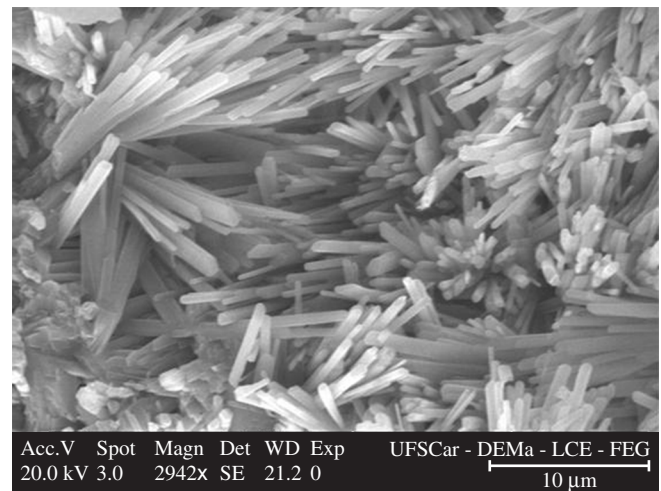


Figure 9. SEM and secondary electron images. Matrix without fibers.

Table 4. Average values of the composites' mechanical properties.

Composite			Water/gypsum ratio		MOR (MPa)		LOP (MPa)		T (kJ.m ⁻²)		MOE (GPa)	
Gypsum (%)	Limestone(%)	Fiber (%)	NG	RG	NG	RG	NG	RG	NG	RG	NG	RG
			90.0	10	-	0.20	-	5.00	-	4.48	-	0.09
			(0.01)		(0.75)		(1.00)		(0.05)		(0.58)	
85.0		5.0	0.27	0.32	10.09	7.75	9.03	6.33	0.80	0.74	9.58	7.43
			(0.01)	(0.01)	(1.25)	(0.86)	(0.87)	(0.96)	(0.13)	(0.20)	(0.97)	(0.79)
82.5		7.5	0.35	0.34	9.71	10.57	6.97	8.25	1.70	1.47	5.94	6.69
			(0.01)	(0.01)	(1.10)	(0.80)	(1.35)	(0.82)	(0.43)	(0.44)	(0.93)	(0.53)
80.0		10.0	0.36	0.37	12.42	11.97	9.21	9.20	2.10	1.86	5.92	5.98
			(0.01)	(0.01)	(1.17)	(0.92)	(1.26)	(0.56)	(0.28)	(0.49)	(0.85)	(0.45)
77.5		12.5	0.37	0.39	13.18	12.63	9.91	9.15	2.27	2.39	5.58	5.05
			(0.02)	(0.01)	(1.34)	(0.45)	(1.48)	(0.56)	(0.33)	(0.34)	(0.89)	(0.34)
75.0		15.0	0.40	0.43	11.66	12.15	7.84	8.47	3.46	3.24	3.88	4.18
			(0.02)	(0.01)	(1.50)	(0.77)	(1.26)	(0.60)	(0.78)	(0.62)	(6.10)	(0.50)

(Standard deviation);

MOR (modulus of rupture); LOP (limit of proportionality); T (fracture toughness);

MOE (modulus of elasticity); RG (recycled gypsum); and NG (natural gypsum).

fibers, and hence, to the increase in the water/gypsum ratio in the proximities of the fibers.

Confirming the superiority of the suction/compression process evidenced in the rupture modulus and toughness results, the simultaneous presence of fiber pullout and fractures indicates the good level of fiber-matrix adhesion (Figure 11).

Crystal incrustations on fiber surfaces and fractured layers with pulled out filaments indicate that the combined work of the phases improves the composite's performance. The cel-cb waste fiber presented good adhesion to the matrix.

3.3. Calorimetry

Unlike the pastes without cellulose (NG100) and (NG90+limestone), the pastes containing 10% of cellulose pulp (NG90+cel-cb) and (NG80+limestone+cel-cb), Figure 12, contributed to increase the "induction time" of the paste, i.e., the time elapsed from

the gypsum's dilution in water to the solution's saturation, which was almost doubled. These results confirm data reported by Zhang¹⁹ and Simatupang & Smith²⁰, whose studies on the action of wood extracts on the setting of gypsum plates found that some substances released by natural fibre fiber in aqueous solution (lignins, resins, polyphenols, oils and fats) interfere in the kinetics of gypsite crystal formation. Cellulose pulp acts as a retardant in the setting process, increasing the induction period and causing displacement of the hydration heat curve of the gypsum paste. In the traditional gypsum paste production and application process, the concept of "useful time" comprises the period from the beginning to the end of the setting time.

Figure 12 illustrates the hydration heat curves (pseudo-adiabatic calorimetry).

The addition of limestone powder did not appear to affect the formation rate of the crystalline gypsite structure, as indicated in Table 5, where the beginning and end of the setting (or hardening)

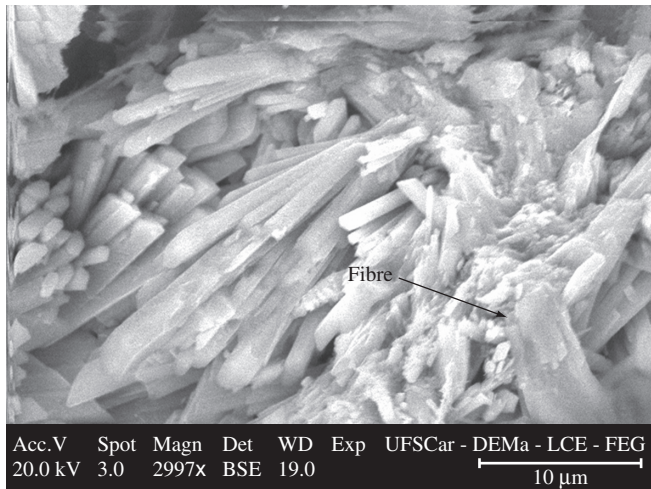


Figure 10. SEM and secondary electron images. Matrix containing 10% of cellulose pulp.

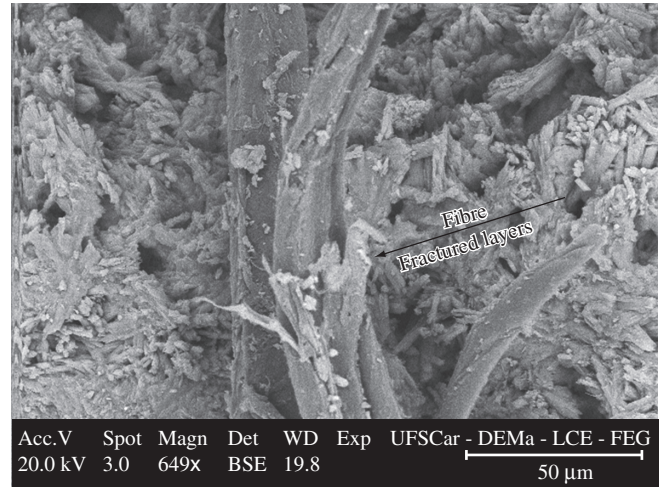


Figure 11. SEM image of fractured fibers.

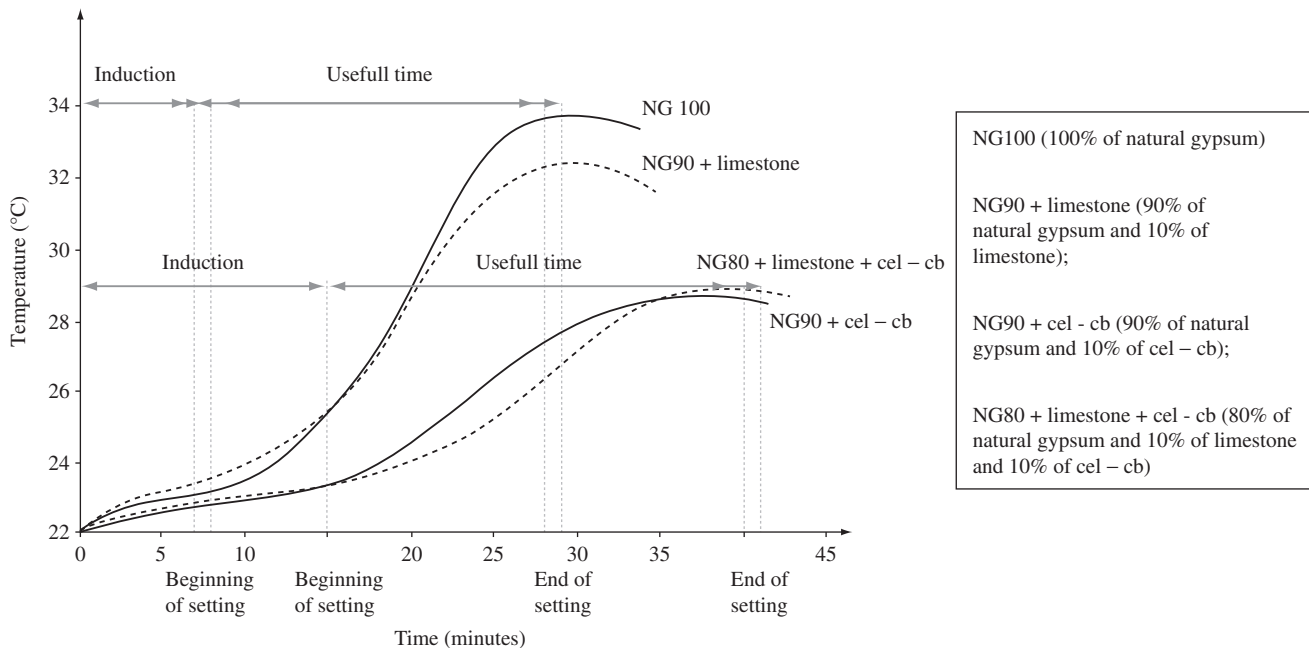


Figure 12. Hydration heat curves obtained with a pseudo-adiabatic calorimeter.

Table 5. Hydration time of the pastes with and without cellulose pulp, and with and without limestone powder.

Time (minutes)	Pastes			
	NG	NG+limestone	NG+cel-cb	NG+limestone+cel-cb
Beginning of the hardening process	7	8	15	15
End of the hardening process	28	29	40	41

time and the useful time were practically identical in the samples with and without cellulose. Based on our experimental results, it can be concluded that the limestone powder acted effectively in reducing the water's surface tension, improving the dispersion of the gypsum mineral and cellulose pulp particles.

4. Conclusions

Compared to the conventional procedure of gypsum plate production, the suction/compression molding process produced composites with high mechanical performance.

The addition of Kraft pulp waste changed the kinetics of gypsum hydration. Comparing gypsum pastes without cellulose pulp (NG 90) to the corresponding pastes with cellulose pulp (NG 80), it is possible to conclude that the cellulose pulp contributed to the increase of induction times in approximately 100%. The natural fibers absorbed and retained a larger amount of water in the matrix, enabling the formation of larger crystals in their proximities. Moreover, the fibers adhered satisfactorily to the gypsum matrix.

All the studied amounts of cellulose pulp waste improved the composites' mechanical performance of the composites. The best results were obtained with 12.5% by mass of cellulose pulp. The specimens with 12.5% of pulp (cel-cb) presented the highest values of modulus of rupture (MOR) around 13 MPa which represent an increase in resistance of 160% approximately compared to their counterparts without fibers.

The stirring vacuum de-watering process originated composites with high mechanical performance. This material is a technically better substitute for brittle gypsum plate, and stands out particularly for its characteristics of high impact strength and high modulus of rupture.

Acknowledgements

The authors are indebted to Furnas Centrais Elétricas' Chemistry Laboratory, to the Construction and Ambiance Laboratory of the University of São Paulo at Pirassununga (FZEA-USP) School of Animal Science and Food Engineering, and to the Pulp and Paper Laboratory of the Federal University of Viçosa's Department of Forest Engineering, MG, for carrying out the tests. Special thanks are also due to Sérgio Santos, Gustavo Tonoli, Zaqueu Dias, Ronaldo Teixeira and José Wilson Nerys for their unstinting help and encouragement.

References

- Agopyan V, Souza UEL, Paliari JC, Andrade AC. *Alternativas para redução do desperdício de materiais nos canteiros de obras*. São Paulo; 1998.
- Moslemi AA. Emerging technologies in mineral-bonded wood and fiber composites. *Advanced Performance Materials* 1999; 6(2):161-179.
- Savastano-Jr H, Agopyan V. Transition zone studies of vegetable fibre-cement paste composites. *Cement and Concrete Composites* 1999; 21(1):49-57.
- Agopyan V. Vegetable fibre reinforced building materials - developments in Brazil and other Latin American countries. In: RN Swamy (Ed). *Natural fibre reinforced cement and concrete. Concrete and Technology and Design*. Glasgow: Blackie; 1988.
- Savastano-Jr H, Warden PG, Coutts RSP. Microstructure and mechanical properties of waste fibre-cemente composites. *Cement and Concrete Composites* 2005; 27(5):583-592.
- Gram HE. Durability of natural fibres in concrete. In: Swamy RN. (Ed). *Natural fibre reinforced cement and concrete*. Glasgow: Blackie; 1988.
- Guimarães SS. Vegetable fiber-cement composites In: 2 *International symposium on vegetable plants and their fibres as building materials*; 1990; Salvador. London: Chapman and Hall; 1990. p. 98-107.
- Savastano-Jr H, Warden PG, Coutts RSP. Brazilian waste fibres as reinforcement for cement-based composites. *Cement and Concrete Composites* 2000; 22(5):379-384.
- Jeulin D, Monnaie P, Péronnet F. Gypsum morphological analysis and modeling. *Cement and Concrete Composites* 2001; 23(2):299-311.
- Ridge MJ. Effect of Temperature on the Rate of Setting of Gypsum Plaster. *Nature* 1959; 184:47-48.
- ASSOCIAÇÃO BRASILEIRA DE NORMAS TÉCNICAS - ABNT. NBR 13207. *Gesso para construção civil - especificação*. Rio de Janeiro; 1994.
- BRITISH STANDARD INSTITUTION. BS 1191: Part 1. *Specification for gypsum building plasters*. London; 1973.
- ASSOCIATION FRANÇAISE DE NORMALIZATION. AFNOR NF B 12-300. *Plâtres: généralités clauses et conditions générales*. França; 1963.
- Cincotto MA, Agopyan V, Florindo MC. O gesso como material de construção - composição química (1ª parte). In: *Tecnologia de edificações*. São Paulo: Pini; 1988.
- RILEM. Technical Committee 49 TFR - Test for the determination of modulus of rupture and limit of proportionality of thin fibre reinforced cement section - *Materiaux et Constructions* 1984; 17(102):441-451.
- Murat M, Jeandot G. Méthodes de mesures et interpretation des effets thermiques associés à l'hydratation des sulfates de calcium et des plâtres industriels. *Revue de Matériaux and Building Research* 1979; 1:264-271.
- Hincapié AM, Cincotto MA. Efeito de retardadores de pega no mecanismo de hidratação e na microestrutura do gesso de construção. *Ambiente Construído* 1997; 1(2):07-16.
- Antunes RPN. *Estudo da influência da cal hidratada nas pastas de gesso*. [Dissertação de Mestrado em Engenharia Civil] São Paulo: Universidade de São Paulo; 1999.
- Zhang, Y. *Influence of wood extractive on hardening and properties of gypsum plaster and gypsum bonded particleboard*. Beijing: Wood Industry; 1990.
- Simatupang MAH, Schmitt U. Wood extractives of rubberwood (*Hevea brasiliensis*) and their influences on the setting of the inorganic binder in gypsum-bonded particleboards. *Journal of Tropical Forest Science* 1994; 6(3):269-285.